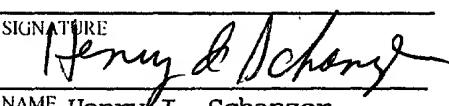


FORM PTO-1390 (REV. 11-2000)		U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE		ATTORNEY'S DOCKET NUMBER
TRANSMITTAL LETTER TO THE UNITED STATES DESIGNATED/ELECTED OFFICE (DO/EO/US) CONCERNING A FILING UNDER 35 U.S.C. 371			U.S. APPLICATION NO. (If known, see 37 CFR 1.5 <b>093763247</b>	
INTERNATIONAL APPLICATION NO. PCT/US00/14652	INTERNATIONAL FILING DATE 26 May 2000		PRIORITY DATE CLAIMED 27 May 1999**	
TITLE OF INVENTION WAVE ENERGY CONVERTERS UTILIZING PRESSURE DIFFERENCES				
APPLICANT(S) FOR DO/EO/US INVENTORS: CARROLL, CHARLES B.; BELL, MEREDITH OCEAN POWER TECHNOLOGIES, INC.:				
Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:				
<p>1. <input checked="" type="checkbox"/> This is a <b>FIRST</b> submission of items concerning a filing under 35 U.S.C. 371.</p> <p>2. <input type="checkbox"/> This is a <b>SECOND</b> or <b>SUBSEQUENT</b> submission of items concerning a filing under 35 U.S.C. 371.</p> <p>3. <input checked="" type="checkbox"/> This is an express request to begin national examination procedures (35 U.S.C. 371(f)). The submission must include items (5), (6), (9) and (21) indicated below.</p> <p>4. <input type="checkbox"/> The US has been elected by the expiration of 19 months from the priority date (Article 31).</p> <p>5. <input checked="" type="checkbox"/> A copy of the International Application as filed (35 U.S.C. 371(e)(2))</p> <ol style="list-style-type: none"> <li><input type="checkbox"/> is attached hereto (required only if not communicated by the International Bureau).</li> <li><input type="checkbox"/> has been communicated by the International Bureau.</li> <li><input checked="" type="checkbox"/> is not required, as the application was filed in the United States Receiving Office (RO/US).</li> </ol> <p>6. <input type="checkbox"/> An English language translation of the International Application as filed (35 U.S.C. 371(e)(2)).</p> <p>7. <input type="checkbox"/> a. <input type="checkbox"/> is attached hereto.</p> <p>8. <input type="checkbox"/> b. <input type="checkbox"/> has been previously submitted under 35 U.S.C. 154(d)(4).</p> <p>9. <input type="checkbox"/> c. <input type="checkbox"/> Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(e)(3))</p> <ol style="list-style-type: none"> <li><input type="checkbox"/> are attached hereto (required only if not communicated by the International Bureau).</li> <li><input type="checkbox"/> have been communicated by the International Bureau.</li> <li><input type="checkbox"/> have not been made; however, the time limit for making such amendments has NOT expired.</li> <li><input type="checkbox"/> have not been made and will not be made.</li> </ol> <p>10. <input type="checkbox"/> d. <input type="checkbox"/> An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(e)(3)).</p> <p>11. <input checked="" type="checkbox"/> e. An oath or declaration of the inventor(s) (35 U.S.C. 371(e)(4)). To be forwarded</p> <p>12. <input type="checkbox"/> f. An English language translation of the annexes of the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(e)(5)).</p> <p>13. <input type="checkbox"/> Items 11 to 20 below concern document(s) or information included:</p> <p>14. <input type="checkbox"/> 11. An Information Disclosure Statement under 37 CFR 1.97 and 1.98.</p> <p>15. <input checked="" type="checkbox"/> 12. An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included. To be forwarded</p> <p>16. <input type="checkbox"/> 13. A FIRST preliminary amendment.</p> <p>17. <input type="checkbox"/> 14. A SECOND or SUBSEQUENT preliminary amendment.</p> <p>18. <input type="checkbox"/> 15. A substitute specification.</p> <p>19. <input type="checkbox"/> 16. A change of power of attorney and/or address letter.</p> <p>20. <input type="checkbox"/> 17. A computer-readable form of the sequence listing in accordance with PCT Rule 13ter.2 and 35 U.S.C. 1.821 - 1.825.</p> <p>21. <input type="checkbox"/> 18. A second copy of the published international application under 35 U.S.C. 154(d)(4).</p> <p>22. <input type="checkbox"/> 19. A second copy of the English language translation of the international application under 35 U.S.C. 154(d)(4).</p> <p>23. <input type="checkbox"/> 20. Other items or information:</p> <p>**The original PCT Application erroneously claimed 5 May 1999 as the priority date.</p>				

U.S. APPLICATION NO. 09/1763247	INTERNATIONAL APPLICATION NO.	ATTORNEY'S DOCKET NUMBER	
21. <input type="checkbox"/> The following fees are submitted: <b>BASIC NATIONAL FEE (37 CFR 1.492 (a) (1) - (5)):</b> Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO. .... \$1000.00 International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO ..... \$860.00 International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee (37 CFR 1.445(a)(2)) paid to USPTO ..... \$710.00 International preliminary examination fee (37 CFR 1.482) paid to USPTO but all claims did not satisfy provisions of PCT Article 33(1)-(4) ..... \$690.00 International preliminary examination fee (37 CFR 1.482) paid to USPTO and all claims satisfied provisions of PCT Article 33(1)-(4) ..... \$100.00		<b>CALCULATIONS PTO USE ONLY</b>	
<b>ENTER APPROPRIATE BASIC FEE AMOUNT =</b>		\$710.00	
Surcharge of \$130.00 for furnishing the oath or declaration later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(c)).		\$130.00	
<b>CLAIMS</b> <b>NUMBER FILED</b> <b>NUMBER EXTRA</b> <b>RATE</b> <b>\$</b>			
Total claims      9 - 20 =      -0-      x \$18.00      \$ -0-			
Independent claims      2 - 3 =      -0-      x \$80.00      \$ -0-			
<b>MULTIPLE DEPENDENT CLAIM(S) (if applicable)</b> + \$270.00      \$ -			
<b>TOTAL OF ABOVE CALCULATIONS =</b> \$840.00			
<input checked="" type="checkbox"/> Applicant claims small entity status. See 37 CFR 1.27. The fees indicated above are reduced by 1/2.      + \$420.00			
<b>SUBTOTAL =</b> \$420.00			
Processing fee of \$130.00 for furnishing the English translation later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(f)).			
<b>TOTAL NATIONAL FEE =</b> \$420.00			
Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31). \$40.00 per property      + \$ -			
<b>TOTAL FEES ENCLOSED =</b> \$420.00			
		<b>Amount to be refunded:</b> \$ -	
		<b>charged:</b> \$ -	
a. <input checked="" type="checkbox"/> A check in the amount of \$420.00 to cover the above fees is enclosed. b. <input type="checkbox"/> Please charge my Deposit Account No. _____ in the amount of \$ _____ to cover the above fees. A duplicate copy of this sheet is enclosed. c. <input type="checkbox"/> The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. _____. A duplicate copy of this sheet is enclosed. d. <input type="checkbox"/> Fees are to be charged to a credit card. <b>WARNING:</b> Information on this form may become public. <b>Credit card information should not be included on this form.</b> Provide credit card information and authorization on PTO-2038.			
<b>NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137 (a) or (b)) must be filed and granted to restore the application to pending status.</b>			
SEND ALL CORRESPONDENCE TO			
<b>HENRY I. SCHANZER, ESQ.</b> 29 BROOKFALL ROAD EDISON, NJ 08817		<b>SIGNATURE</b>  <b>NAME</b> Henry I. Schanzer 25,219	
<b>REGISTRATION NUMBER</b>			

## Wave Energy Converters Utilizing Pressure Differences

### Background of the Invention:

This invention relates to the conversion of energy from naturally occurring sources of mechanical energy, and particularly to the conversion of the mechanical energy present in ocean surface waves to useful energy, particularly electrical energy.

In many known systems for capturing surface wave energy, a float is used for being vertically oscillated in response to passing waves. The float is rigidly coupled to an energy converter which is driven in response to vertical movements of the float. In one system, described in U.S. patents 4,773,221 and 4,277,690 (the subject matter of which is incorporated herein by reference), an open-ended hollow tube is rigidly suspended beneath a float, the tube being completely submerged and in vertical orientation.

The tube vertically oscillates in the water in correspondence with movements of the float and, in the absence of anything within the tube, the tube moves freely relative to the column of water within the open-ended tube. In one embodiment, a movable piston is disposed within the tube for blocking relative movements between the water column and the tube. As the tube and float oscillate within the water, the mass of water within the tube tends to block corresponding movements of the piston, hence the piston moves relative to the tube. Actual movements of the piston do

occur, however, and provided the entire system is oscillating at its natural resonant frequency, relatively large amplitude oscillations of the piston can occur. The moving piston drives an energy converter fixedly mounted, e.g., within the float, for converting the piston movements to useful energy.

While these float driven tube systems work, efficient operation requires that the natural resonant frequency of the system closely matches the frequency of the ocean waves driving the system. While this can be generally accomplished at a specific site and specific time, particularly if means for adjusting the resonant frequency of the system in response to changing surface wave frequencies are provided, a problem is that, at any instant, multiple random surface waves are present whereby much of the wave energy present can not be efficiently transferred to the oscillating system. Also, the means for adjusting the resonant frequency of the device generally involves changing the water mass within the device. Since this mass is quite large, it is not readily changed.

A feature of the present invention is that a relatively high efficiency of operation is obtained which is relatively insensitive to random variations of wave frequencies and amplitudes.

### **Summary of the Invention:**

In a first embodiment of the invention, an open-ended, hollow tube is disposed in vertical, submerged and fixed location relative to the mean water level. Specifically, the tube is not in "floating" (moveable) relationship with the passing waves. The length of the tube and the depth

of the top end of the tube beneath the mean water level are selected, as described hereinafter, depending upon the frequency and amplitude of the most prevalent anticipated surface waves, as well as the water depth. While maximum efficiency of operation is attained when the anticipated waves are present, the fall-off of efficiency of operation is relatively small with variations of wave conditions.

During operation, pressure variations, at the top, open end of the tube (caused by passing waves) in comparison with a relatively fixed pressure at the open, bottom end of the tube (unaffected by passing waves) cause vertical flows of water through the tube which are used for driving an energy converter, preferably by means of a movable piston within the tube.

In a second embodiment of the invention, a hollow tube having a closed top end and a bottom open end is disposed in vertical, submerged but relatively movable relation with the mean water level. In a preferred embodiment, the tube is secured for vertical cyclical movements relative to a float fixedly submerged beneath the water surface and disposed within the tube. The dimensions of the tube and its at-rest location relative to the water surface are in accordance with the tube of the first embodiment except, in the second embodiment, the piston movable within the tube of the first embodiment comprises the closed top end of the tube of the second embodiment. During operation, pressure variations against the top end of the tube cause vertical oscillations of the tube relative to the fixed float, and such oscillations are used for driving an energy converter fixed

within the float and coupled to the movable tube. In a variation of the second embodiment, the transducer is not mounted in a float but fixedly secured to the ocean bottom. The movable tube, which need not be hollow, is secured to the transducer

In all embodiments, movements of the tube relative to the adjoining water are caused not by wave-induced displacements of a float on the water surface, but in response to pressure variations caused by passing waves.

#### **Description of the Drawings:**

The drawings are schematic and not necessarily to scale.

FIGURE 1 is a sketch for identifying various relevant dimensional parameters of a system according to the present invention deployed in a body of water;

FIGURES 2, 2A and 3-6 are side sectional views showing different embodiments of power converting systems in accordance with a first embodiment of the present invention deployed in bodies of water, e.g., an ocean;

FIGURE 7 is a side elevational view of an energy converter in accordance with a second embodiment of the invention;

FIGURE 8 is an end view of the converter looking in the direction of the arrows 8-8 in Fig. 8;

FIGURE 9 is an isometric view of the converter shown in Figs. 7 and 8; and

FIGURE 10 is a side elevational view of a modified version of the embodiment shown in Figs. 7-9.

#### **Description of Preferred Embodiments of the Invention:**

An apparatus according to a first embodiment of the present invention is shown in Figure 1. Shown schematically is an open-ended tube 10 disposed (as herewith described) in fixed, vertical orientation below the mean water level of a body of water, e.g., an ocean having wind driven surface waves. Figure 1 also identifies parameters important in the practice of the invention, i.e., wave height, wave length, water depth, depth of the top of the tube below the water surface, length of the tube, and the diameter of the tube. The optimum depth for the lower end of the tube is dependent on the wavelength ( $\lambda$ ) of the longest waves to be utilized in an efficient manner. The principle of operation is that the changes in water energy level, which can be expressed as changes in pressure, due to the passage of wave peaks and troughs, is highest near the surface, and these pressure changes decay exponentially with depth below the surface. Thus, the top of a long tube experiences relatively large pressure variations while

the bottom of the tube experiences an almost steady pressure that is equal to the pressure due to the weight of water above it at the mean water level.

The energy levels at different water depths under a wave field can be calculated with Equations 1 and 2. The equations are for deep water waves and are modified somewhat by the depth in more shallow water (depths less than  $\lambda/2$ ). The water energy levels due to waves of a given size are a function of wave length and water depth. There is little practical value in extending the tube bottom any deeper than 1/2 the wavelength of the longest waves to be optimally used because the energy level is already greatly reduced from its near surface value.

$$E_d = E_s \exp(-2\pi d/\lambda) \quad (1)$$

where:  $E_s$  is the energy due to a wave at the water surface, and  
 $E_d$  is the energy due to a wave at a depth equal to  $d$ , and  
 $\lambda$  is the wave length of the waves being considered

The wave length of deep water waves may be calculated by the formula:

$$\lambda = gT^2/2\pi \quad (2)$$

where:  $g$  is the gravitational constant, 9.8 meters per second per second, and  
 $T$  is the period of the waves in seconds

As an example using equation 2, for waves with a period of 7 seconds, the wave length is

$$\lambda_7 = 76.43 \text{ meters}$$

As a second example, for waves with a period of 5 seconds, the wave length is

$$\lambda_5 = 38.99 \text{ meters}$$

For waves with a period of 7 seconds and a wave length of 76.43 meters, and waves with a period of 5 seconds and a wave length of 38.99 meters, the energy at different depths can be calculated as percentage of the energy at the surface, using Equation 1. This is shown in Table 1.

**Table 1.**

<u>energy water depth (m)</u>	<u>depth as a % of <math>\lambda_7</math></u>	<u><math>E_{d7}</math> as % of <math>E_s</math></u>	<u>depth as a % of <math>\lambda_5</math></u>	<u><math>E_{d5}</math> as % of <math>E_s</math></u>
0.1	0.1	99.2	0.3	98.4
0.5	0.6	96.0	1.3	92.3
1.0	1.3	92.1	2.6	85.1
19.1	25	20.8	49	4.6
38.21	50	4.3	98	0.2
76.43	100	0.2	196	0

Table 1 shows that when waves with a period of 7 seconds are present, and the tube 10 has its top end at depth of 0.5 meters below the surface, and its bottom end at a depth of 38.21 meters below the surface, the top will experience pressure changes 91.7% (96 - 4.3) larger than the bottom. These conditions will cause water to flow down the inside of the tube when a wave peak is over the top end, and water to flow up the inside of the tube when a wave trough is at the top of the tube. This pressurized water flow provides the opportunity to extract mechanical power from the wave energy. Extending the tube from 38.21 meters to 76.43 meters in length only increases the pressure differential by 4.1% (4.3 - 0.2).

Further study of the Table 1 shows that when waves with a 5 second period are present, a tube with its bottom at 38.21 meters below the

surface has an even lower pressure variation at the bottom, 0.2%, than when 7 second period waves are present. Thus wave energy from shorter wave length and shorter period waves can be collected efficiently. When waves of longer period are present, the energy, or pressure variations, at the tube bottom gradually increase. Thus, the efficiency of energy collection will gradually decrease. However, the range of efficient operation is much larger than in the previously described known devices that are tuned for specific wave periods for resonant and efficient operation. These devices can suffer a significant loss of efficiency when the wave period changes even a few seconds.

Table 1 also shows that as the wave period decreases, the importance of the top of the tube being near the surface increases. For example, with a water depth of the top of the tube being 0.5 meters under the surface in 7 second period waves, the energy has decreased at the tube top to 96% of its maximum, while in 5 second waves the energy has decreased to 92.3% of its maximum.

Regular waves are waves that have a consistent period. A sine wave is an example of a regular wave. Regular waves at a constant period would allow the tuning of a resonant wave energy capture device to the specific wave period, even though the wave period may change with the negative impact mentioned above. In practice, ocean and sea waves are both random and irregular and simultaneously contain waves with different periods. An example of this is a case when ocean swells with a 10 second period are present along with wind waves with a 5 second period. The inventive apparatus has the ability to capture energy efficiently from

irregular waves as well as from regular waves. This is because the apparatus is not optimized for a specific period but is driven dependent upon the instantaneous quantity of water above or below the mean water level (but subject to “cancellation effects” discussed hereinafter).

The theoretical amount of energy that can be captured at a site with a given water depth and wave characteristics can be determined as follows. Bernoulli's Equation for fluids in unsteady irrotational flow is:

$$\frac{\delta\phi_1}{\delta t} + \frac{P_1}{\rho} + gy_1 + \frac{V_1^2}{2} = \frac{\delta\phi_2}{\delta t} + \frac{P_2}{\rho} + gy_2 + \frac{V_2^2}{2}$$

Where (1) is a point in the fluid and (2) is another point in the fluid, and where:

$\delta\phi/\delta t$  is the differential of the velocity potential in meters squared per second squared ( $m^2/s^2$ ), at a point, and  
 $gy$  is the gravitational constant times the depth at a point in  $m^2/s^2$ , and  
 $P/\rho$  is the pressure at a point divided by the fluid density in  $m^2/s^2$ , (to achieve these dimensions it should be remembered that mass can be expressed as force divided by acceleration), and  
 $V^2/2$  is the velocity squared of the fluid at that point  $m^2/s^2$ .

For example, if point 1 is considered to be near the water surface as is the top of the tube, and point 2 is deeper as is the bottom of the tube, the Bernoulli Equation can be the basis for analysing the different forms of energy available at each point as time passes.

**Principle of Operation - Energy Capture:** The simple long tube described above provides a situation where there are two different pressure levels appearing simultaneously at each end of the tube. Two

preferred methods of capturing energy from the available energy in the tube are as follows:

1. A piston 12, shown in Figure 2, placed in the tube is forcefully driven up and down by water in the tube moving up and down due to the varying pressure differentials above and below the piston. This forceful movement is converted to mechanical power by attaching a device to the piston that resists its movement. One example is the rod of a hydraulic cylinder. The motion of the cylinder rod pumps a pressurized fluid (hydraulic fluid) through a hydraulic motor which then rotates. The mechanical power produced by the hydraulic motor is converted to electrical power by a generator attached to the motor. In Figure 2, the water driven piston 12 and its shaft are shown to move up and down while guided by the Piston Shaft Support and Shaft Bearings 16. To reduce mechanical drag on the system the piston preferably does not touch the sides of the tube. A clearance between the piston rim and tube of 3 to 6 millimeters will permit some water to leak past the piston. This represents a loss of power but is a small percentage of the area for a piston that is larger than 1 meter in diameter. A hydraulic cylinder rod 18 (from a hydraulic cylinder 20) is attached to the top of the piston shaft 12. A hydraulic cylinder support 22 fixedly attaches the cylinder 20 to the tube 10. Hydraulic hoses 24 carry the hydraulic fluid back and forth to a watertight compartment that contains an hydraulic motor and electric generator. A double-ended cylinder (rod extends from both ends) is preferred because the cylinder performance is the same in both stroke directions. The piston is made buoyant enough to cause the piston - piston shaft - hydraulic

cylinder rod assembly to be neutrally buoyant, and therefore move up or down equally with the same applied forces. A preferred arrangement of the components is shown in Figure 2A. In this arrangement, the piston 12 slides up and down on the hydraulic cylinder itself. Both ends of the hydraulic cylinder rod 18 are fixedly attached to the tube 10 by the hydraulic cylinder rod supports 22. A watertight compartment 26 is part of the piston assembly and contains the hydraulic motor and electric generator. This compartment is buoyant enough to cause the entire piston assembly to be neutrally buoyant.

Figure 2 also shows an arrangement for mooring the power converting system. This is later described.

Figure 3 shows an arrangement where the area of the piston 12 is larger than the area of the tube 10 at its top and bottom ends. This is to illustrate that the piston area can be either larger or smaller than the tube end areas. In a given situation, the arrangement in Figure 3 will produce a higher force and a shorter stroke than if the piston and tube ends have the same area. This is because the tube length and depth determines the pressure differential on the piston, and the tube end areas determine the volume of water flow. Thus, the same pressure on a larger piston area produces more force, but more water volume is required to move the larger piston. Figure 3 illustrates that the piston size can be varied to match desired piston forces and strokes. However there are losses of energy incurred whenever the moving

water is caused to change direction as it does when the piston area is different than the tube end areas. Thus, the most energy efficient configuration is when the piston and tube ends have the same area.

A second power take-off approach (not illustrated) is to attach a rod to the piston that moves vertically with the piston. Instead of this piston rod being attached to a hydraulic cylinder, it is attached to a positive drive belt (the belt and sprockets having teeth that are positively engaged), that is around two vertically arranged sprockets. As the piston is driven up and down by the wave energy it drives one side of the belt up and down causing the sprockets to rotate. One of the shafts of a driven sprocket is coupled to a generator to produce electric power.

A third power take-off approach (not illustrated) is to directly drive a linear generating device, such as a linear electric motor, with the piston movement. Due to the sub-surface marine environment, the hydraulic approach is preferred.

2. In the system shown in Figure 4, a turbine 40 is disposed within a tube 10 for being driven to rotate by the water flow in the tube moving up and down due to the varying pressure differential at the top and bottom of the tube. This rotation produces mechanical power by, for example coupling the shaft of an electric generator 42 to the turbine shaft 44. The tube preferably has, as shown, large diameter ends, and a small diameter turbine section in order to increase the water flow velocity through the turbine.

The moving piston approach (1) is preferred because in general, the inventive systems are more readily designed for providing powerful strokes of limited length rather than providing rapid water flow. Each approach is described in more detail below:

**1. Moving piston approach:** As a piston such as shown as 12 in Figs. 2, 2A, and 3 moves against resistance it produces a force (Newtons). The piston moves a certain distance in a given time (meters per second). The product of this force times velocity is Newton-meters per second (Nm/s) which converts directly to watts of power. One Nm/s is equal to one watt.

$$\text{Power}_{\text{watts}} = \text{Force}_{\text{Newtons}} \times \text{Velocity}_{\text{meters/second}} \quad (3)$$

A longer stroke in a given time at a lower force can produce the same amount of power as a shorter stroke in the same time at a higher force, or vice versa. In practical applications of the piston approach, there is a limit on the length of piston stroke allowed. This is because practical devices such as a hydraulic cylinder have a certain amount of stroke, and exceeding that physical limit damages the cylinder. Also, in a given location, the waves are normally in a known range of sizes during the year. Thus, it would be economically impractical to provide equipment that could stroke farther than would be caused by the normally present waves. Prevention of damage by larger than normal waves, such as storm waves (not illustrated), is by pressure relief doors in the tube 10 above and below the pistons 12 range of motion. If a wave produces a pressure differential (and resulting piston force) across the piston that is more than a

preselected valve, the doors are pushed open. This allows water to bypass the piston, reducing its force and preventing damage to the device.

A piston system will normally have provision for a certain physical stroke range such as 1 meter, but could be longer or shorter. However, the force can be increased or decreased by simply making the unit and its piston larger or smaller. This is an important factor in the design of a practical system, and is based on the fact that fluid pressure does not depend on the size of the area it is acting upon. For example, assume that waves are expected to be present that provide an average pressure differential of 2,000 Pascals (Pa) between the top and the bottom of the tube, as described above. A Pascal is a pressure of one Newton per square meter. Also, assume that the waves have a period of 5 seconds, that is, a wave will move from a peak to a trough in 2.5 seconds. If the piston stroke is limited to 1 meter, and it is moving its full stroke, it will have an average velocity of  $1/2.5 = 0.4 \text{ m/s}$ . If 1000 watts, or  $1000 \text{ Nm/s}$ , is desired from the system, then the average force must be  $(1000 \text{ Nm/s})/(0.4 \text{ m/s}) = 2,500 \text{ N}$ . Since the pressure differential is 2,000 Pa or  $2,000 \text{ N/m}^2$ , the piston area must be  $(2,500 \text{ N})/(2,000 \text{ N/m}^2) = 1.25 \text{ m}^2$ . This corresponds to a piston diameter of 1.26 meters (D).

The mass of water in the tube and piston area moves along with the piston. It must be accelerated in one direction, decelerated to a stop, accelerated in the other direction, decelerated to a stop, and so on. Therefore, some of the force produced by the pressure differential on the piston must be used to accelerate the water mass. This can be calculated as force equals mass times acceleration, or  $F_{\text{water}} = m_{\text{water}}a$ . Some of this

force is recoverable from the decelerating water. However, having to accelerate and decelerate a large water mass causes the optimum tube 10 length to be shorter than  $\frac{1}{2}$  the waves length. This is because a longer tube captures a higher pressure differential than a shorter tube, but also contains more water. The optimum tube 10 length can be calculated for a specific wave length, wave height, and water depth using Bernoulli's Equation as previously discussed.

By way of concise summary, characteristics of the moving piston approach are:

1. A tube long enough to create a significant varying pressure differential between its top and bottom ends when placed in waves with a range of wavelengths.
2. A piston within the tube that causes the varying pressure from the top of the tube to occur at the top surface of the piston, and the relatively constant pressure from the bottom of the tube to occur on the bottom surface of the piston.
3. Because of 1. and 2. the piston is driven up and down with force and velocity.
4. A means, such as a hydraulic cylinder and motor, to convert the reciprocating mechanical power of 3. into rotary mechanical power.
5. An electric generator to convert the rotary mechanical power of 4. into electrical power.

6. The piston diameter can be larger or smaller than the tube diameter, producing either a relatively high force low velocity motion or a relatively low force high velocity motion.
7. The sizes of the system tube and piston components affect the amount of water mass enclosed within the system which affects the amount of acceleration of the piston and water that can be achieved from a given wave environment.

Additional requirements, discussed further hereinafter, are:

8. The system can utilize a fixed mooring to the sea bottom, or a mooring that provides a floating unit to balance the piston forces with a properly sized buoyant section.
9. The system can utilize a mooring that combines a fixed buoyant mooring and additional buoyancy to compensate for tidal variations by moving the tube top up and down with the tide.

Various mooring arrangements are described hereinafter.

2. Description of turbine approach: The principles of operation of units that use a water turbine instead of a moving piston for power extraction are very similar. The key difference is the need for a high water flow velocity. As shown in Equation 3, force and velocity make equal contributions to power output.

$$\text{Power}_{\text{watts}} = \text{Force}_{\text{Newtons}} \times \text{Velocity}_{\text{meters/second}} \quad (3)$$

The moving piston approach must limit the stroke and hence the velocity for practical reasons. Thus, the force is emphasized by providing a large piston area. When using a turbine to extract power from flowing fluids a high velocity is desirable to overcome initial static friction to insure that the turbine starts rotating, and to provide efficient operation. The power available for capture from a cross sectional area of fluid flow is given by:

$$\text{Power}_{\text{watts}} = 0.5 \times A \times \rho \times V^3 \quad (4)$$

Where A is the cross sectional area of flow in  $\text{m}^2$ ,  $\rho$  is the density of the fluid (1000  $\text{kg/m}^3$  for water), and V is the velocity in meters per second.

A high average velocity is desirable to optimize power output. The maximum thrust, or force, on a turbine in fluid flow is given by:

$$\text{Thrust}_{\text{Newtons}} = (3/8) \times A \times \rho \times V^2 \quad (5)$$

Once the velocity profile has been determined for a certain tube configuration and wave profile, the expected power output can be calculated from Equation 4. Also, the necessary buoyancy volume to balance the thrust force and maintain stationary position for the tube can be calculated from Equation 5.

Mooring of the above-described embodiments is now described.

In the example shown in Figure 2, a mooring attachment to the sea bottom is shown. The mooring attachment acts as a mechanical datum to resist the upward and downward forces of the piston and keeps the tube fixed in place. The mooring attachment must be strong enough to withstand the downward forces produced by the unit, and heavy enough to resist the upward forces produced by the unit. It must be strongly attached to the ocean bottom to resist the forces produced by storm waves.

In other sites the water may be too deep for practical bottom mounting. Figure 5 shows an arrangement for mooring the inventive systems in virtually any depth of water because the length of its mooring chain 17 is variable. The tube 10 is held in vertical position by buoyancy tanks 50 attached to its outer perimeter. These buoyancy tanks are sufficiently buoyant to float the unit to the surface were it not held by its mooring chain or cable. The tanks are buoyant enough to support the weight of the unit plus at least the maximum downward force exerted by the piston against the tube. This prevents the tube from moving lower during normal operation of the power producing tube. The mooring chain must be at least strong enough to resist the net upward force of the buoyancy tanks, plus the maximum upward force produced by the piston against the tube. The anchor also must weigh at least as much as the net upward force of the buoyancy tanks plus the maximum upward force produced by the piston against the tube to prevent lifting of the anchor.

The fixed depth mooring arrangements shown in Figures 2 and 5 will allow tidal changes in water depth to affect power capturing performance.

In normal tides, for example 1 meter, the effect is small. A preferred mooring plan is to moor the unit at its planned depth below the surface at the midpoint of the tidal change. Then some times it will be deeper below the surface (high tide), and some times it will be closer to the surface (low tide) than planned. Table 1 indicates that the energy level at the top of a tube that is 1 meter below the mean surface of waves with a 7 second period is 4% less than if it were 0.5 meters below the mean surface. Thus a unit that was moored 1 meter below the surface at mid-tide in a 1 meter tidal environment would range from plus or minus 0.5 meters from the planned depth during a day. A unit moored so shallow that wave troughs expose the top of the unit suffers little or no loss in power output. Therefore, such a unit fixedly moored as discussed above will produce approximately at its average planned level in a normal tidal environment. In areas with high tides, the unit is preferably mounted lower in the water to prevent excessive exposure during wave troughs. This will reduce the average power that the unit can capture as can be estimated from Table 1. To meet a certain power goal, a slightly larger unit is required than if the site had smaller tidal changes. The simplicity of a fixed mooring arrangement generally outweighs the power loss in sites with range of depths and tides that are not extreme.

A second mooring approach, shown in Figure 6, combines a fixed bottom mounting and a floating tube top. The fixed bottom mounting provides the simplicity discussed above, and the float provides tidal compensation. In this case, the top portion of the tube 15 is flexible and can be extended upward by the buoyancy of a small float 62 when the tide

is high and raises the mean water level. When the tide is low, the float 62 follows the water level downward compressing and shortening the flexible top tube section 15. The float maintains the top of the tube at a relatively fixed depth below the water surface, e.g., 1 meter. The apparent change in the water height above the tube is approximately the same whether the water is rising and falling above a fixed open tube top, or is rising and falling above the tube extension. In this arrangement, the large forces produced by the piston working in its pressure driven mode are countered by the fixed mooring buoyancy tanks 50, while the added buoyancy tanks 62 only raise and lower the top of the tube.

A second embodiment of the invention, illustrated in Figures 7 through 9 is now described.

Figures 7-9 show a hollow tube 110 having a closed top end 112 and an open bottom end 114. As previously described in the first embodiment, the tube 110 is in vertical, submerged orientation but, unlike the tube 10 in the first embodiment, which is preferably fixed in place, the tube 110 of the second embodiment is vertically movable relative to a fixed support. Such support can be a rigid structure mounted on the water bed, but, especially in deep water, is preferably a float 116 fixedly moored to the water bed 118 by an anchor 120 and a chain or cable 128.

Most conveniently, the tube 110 encloses the float 116 and, because the tube is vertically elongated, the float 116 is similarly elongated.

The float 116 has a large buoyancy, and corresponds to a fixed structure rigidly mounted on the water bed but with the exception that some horizontal displacement of the float can occur in response to horizontal water movements. Such horizontal displacements of the float will generally occur at a slow rate and, essentially, the function of the float is to provide a definite position of the tube relative to the water bed. In situations where large changes in the water level occur, means, generally known, are used for adjusting the distance between the float and the water bed for maintaining a fixed distance between the float and the water surface. However, and as explained in the description of the first embodiment, power generation is relatively insensitive to moderate water level changes and, typically, the float is positioned for optimum performance at the average water level and not thereafter changed in position with water level changes.

The tube 110 is secured to the float 116 by means of a hydraulic pump 122 of known type comprising a rigid casing 124 with a piston rod 126 (for pumping fluids within the pump) extending entirely through and outwardly from both ends of the casing 124. Herein, the pump casing 124 is rigidly secured to the movable tube 110 by a spoke-like bracket 121 (so as not to impede water movement within the tube 110). The upper end of the pump casing 124 is rigidly secured to the closed top end of the tube 110 but with one end 126b of the piston rod 126 extending through the tube end. (Optionally, a navigation aide 127 is attached to the rod end 126b and extends above the surface of the water.) The other end 126a of the piston rod 126 is rigidly secured to the float 116. The tube is neutrally

buoyant and includes a hollow buoyancy chamber 125. Being neutrally buoyant, the tube 110 vertically oscillates in response to tube top-to-bottom pressure variations caused, as previously described, by passing waves. Vertical oscillations of the tube 110 relative to the fixed float 116 thus cause relative movements between the pump casing 124 and the pump piston rod 126, the result being the generation of alternating hydraulic pressures within the pump which can be used for pressure circulating a fluid through hoses 111a for driving a hydraulic motor-electrical generator 111.

Factors influencing the design of the overall system are similar to those described in the description of the first embodiment. Therein, a piston within a stationary tube moves in response to passing waves. Herein, the closed (upper) end 112 of the tube 110 functions as a piston movable relative to a fixed support.

During operation, the tube upper end 112 remains submerged for all passing waves within a range of wave sizes with which the system is designed to operate. For avoiding excessive forces due to extra large waves, pressure relief valves are used, e.g., in the form of spring biased doors 130 shown in Fig. 10 at the top end 112 of the tube 110. Herein, four doors 130 are shown. If the pressure differential between the water above the tube and the water inside the tube exceeds a preselected level, two of the doors open downwardly to equalize the pressure within and outside the tube 110. The other two doors 130 open upwardly to relieve internal excess pressures due to excessively deep wave troughs passing

over (or beneath) the tube upper end 112. The spring bias for the doors 130 can be obtained from weights or buoyant compartments on the doors.

An advantage of the cable anchored arrangement shown in the figures is that the unit is free to move horizontally due to wave action. This reduces the horizontal forces imposed on the mooring and reduces the mass of the required mooring. Large horizontal movements tend to lower the tube upper end 112 relative to the water surface. This lowering tends to reduce the output power from the unit otherwise obtainable when the tube upper end 112 is optimally spaced beneath the water surface (previously described). However, as previously noted, changes in power production with increased spacings of the tube end from the water surface are rather gradual, and useful power production continues even with large horizontal leanings of the unit.

Relative horizontal movements between the float 116 and the tube 110 are preferably avoided for avoiding damage of the mechanical coupling therebetween. For such movements to occur, in response to lateral movements of the tube 110, water must move within the tube 110 from side to side of the float 116. Such water movements, and attendant relative lateral movements of the float 116 relative to the tube 110, are essentially prevented by the use of vertically elongated, radially extending fins 117 shown in Figs. 8 and 9.

The above-described arrangement of a float 116 within a tube 110 provides a self-contained unit which can be readily assembled on-shore

and transported for simple placement at an ocean site. In such arrangement, the float 116 serves as a fixed support on which a transducer is fixedly mounted; the transducer, in turn, being connected to and driven by the movable tube 110.

In an alternate arrangement, shown in Fig. 10, a transducer 222 (e.g., a hydraulic tube or the like) is fixedly mounted on the floor of the ocean (preferably by a mechanical coupling, e.g., a ball-socket joint 232, allowing pivoting of the transducer 222), with the movable piston rod 226 of the transducer rigidly connected to the bottom end of a neutrally buoyant tube 210 identical to the tube 110 shown in Figs. 7-9 but not including an internal float. The tube 210 is connected to the piston rod 226 (again, preferably by a pivoting coupling) by an anchoring link 228 which can be an anchor chain or, preferably, a solid rod having a high modulus of elasticity, i.e., low straining with applied stress.

In the very first patent (USP 4,404,490) issued to the owner of the present invention, reference is made to "cancellation effects", i.e., the energy robbing effect when the dimensions of the wave energy collector are a significant fraction of the wave length of the surface waves (the subject matter of such patent being incorporated herein by reference). Herein, for example, top to bottom pressure variations across the lengths of the various herein disclosed tubes occur in response to passing waves. If, for example, the diameter of the tubes were equal to the wave lengths of the passing waves, the pressure increases caused by the wave crests overlying the tube top ends would be cancelled by the simultaneous

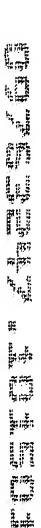
presence of the overpassing wave troughs. Thus, no vertical oscillations of the tubes would occur. Ocean waves, however, tend to be quite large and, for practical reasons, the diameter of the tubes are so small in comparison with the wave lengths that cancellation effects can be ignored – provided that the tube diameters are not in excess of a relatively small proportion of the wave length, e.g., 10%.

Any such cancellation effect occurs in directions parallel to the directions of movements of the waves. No cancellations occur in directions normal to the wave directions, hence quite large area tubes can be used of rectangular cross-section provided the axis of greater length (in excess of 10% of the wave length) is maintained perpendicular to the wave direction.

With, in the embodiment shown in Fig. 10, the transducer 222 disposed below and outside the tube 210, a hollow space within the tube 210 for containing the transducer 222 and a float 116 (as in Fig. 7) is not required, and the tube 210 need not be hollow and need not have an open bottom end. The only requirements for the tube 220, in accordance with the present invention, are that it is similar to the tube 110 in that it has the same outside dimensions (for use with the same wave environment) and has a closed top end serving as a piston responding to surface wave pressure variations. The tube 220, similarly as the tube 110, must be neutrally buoyant, for vertical oscillations in responses to top to bottom pressure variations caused by overpassing waves, but the tube can be hollow or solid to any extent as may be desired.

**What is claimed is:**

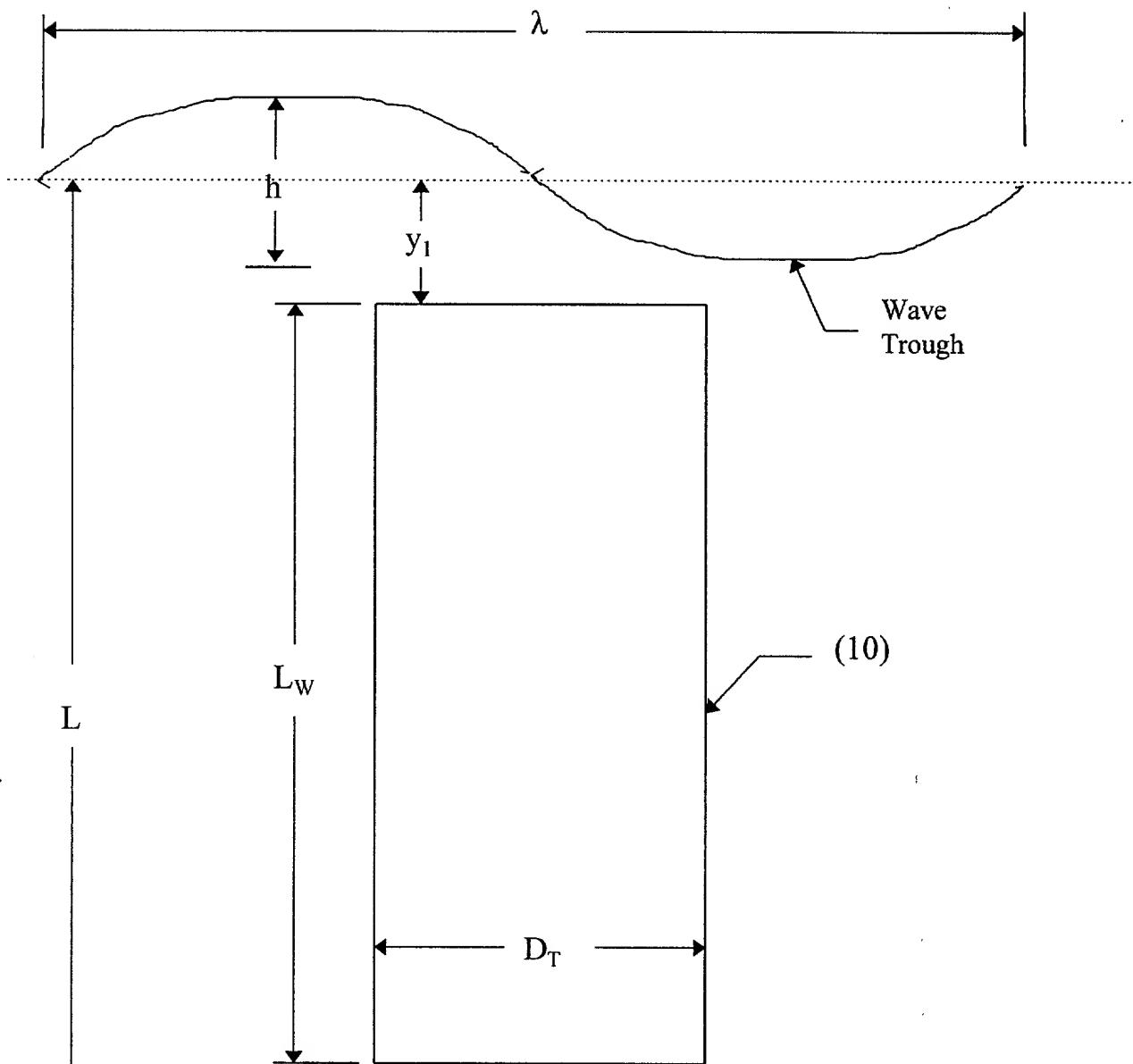
1. An apparatus for capturing energy from preselected surface waves on a body of water, the waves varying from a maximum to a minimum wavelength and having a maximum amplitude above and below a mean water level present during the passage of said waves, the apparatus comprising an elongated cylinder mounted in vertical and completely submerged orientation relative to said mean water level, the cylinder terminating at a top end structurally spaced from the water surface and disposed, in the absence of surface waves, at a first depth approximately equal to said maximum amplitude, and the cylinder having a bottom end disposed at a second depth where the energy level associated with waves at said maximum wavelength is a small percentage of the energy associated with said maximum wavelength waves at said mean water level, and the cylinder including a barrier to water flow through the cylinder for converting movements of the water relative to said cylinder to captured energy.
2. An apparatus according to claim 1 wherein the said second depth is equal to about 50% of said maximum wavelength waves.
3. An apparatus according to claim 1 wherein said cylinder is hollow has an open top end and is fixedly mounted relative to said mean water level, and said barrier comprises a piston slidably disposed within said cylinder and connected to an energy converter,



4. An apparatus according to claim 1 wherein said cylinder has a closed top end serving as said barrier, and said cylinder is slidably connected to an energy converter.
5. An apparatus according to claim 4 wherein said energy converter is fixedly mounted on a float fixedly secured to a floor of the water body.
6. An apparatus according to claim 5 wherein said float and said energy converter are disposed within said cylinder.
7. An apparatus according to claim 4 wherein said energy converter is fixedly secured to the floor of the water body and said cylinder is rigidly coupled to said energy converter.
8. A method for capturing energy from preselected surface waves on a body of water, the waves varying from a maximum to a minimum wavelength and having a maximum amplitude above and below a mean water level present during the passage of said waves, the method comprising disposing in said body of water an elongated cylinder in vertical and completely submerged orientation relative to said mean water level, the cylinder having a top end structurally disconnected from the surface of the water and disposed at a first depth approximately equal to said maximum amplitude, and the cylinder having a bottom end disposed at a second depth where the energy level associated with waves at said maximum wavelength is a small percentage of the energy associated with said maximum wavelength waves at said mean water level, and disposing

within the cylinder a barrier to water flow through the cylinder in response to cylinder top to bottom water pressure differentials caused by said passing waves for converting movements of water relative to said cylinder to captured energy.

9. A method according to claim 8 wherein the said second depth is equal to about 50% of said maximum wavelength waves.



$h$  = wave height - peak to peak

$\lambda$  = wave length

$L$  = water depth

$y_1$  = depth of tube below mean water level

$L_W$  = length of tube

$D_T$  = diameter of tube

Ocean Bottom

Figure 1

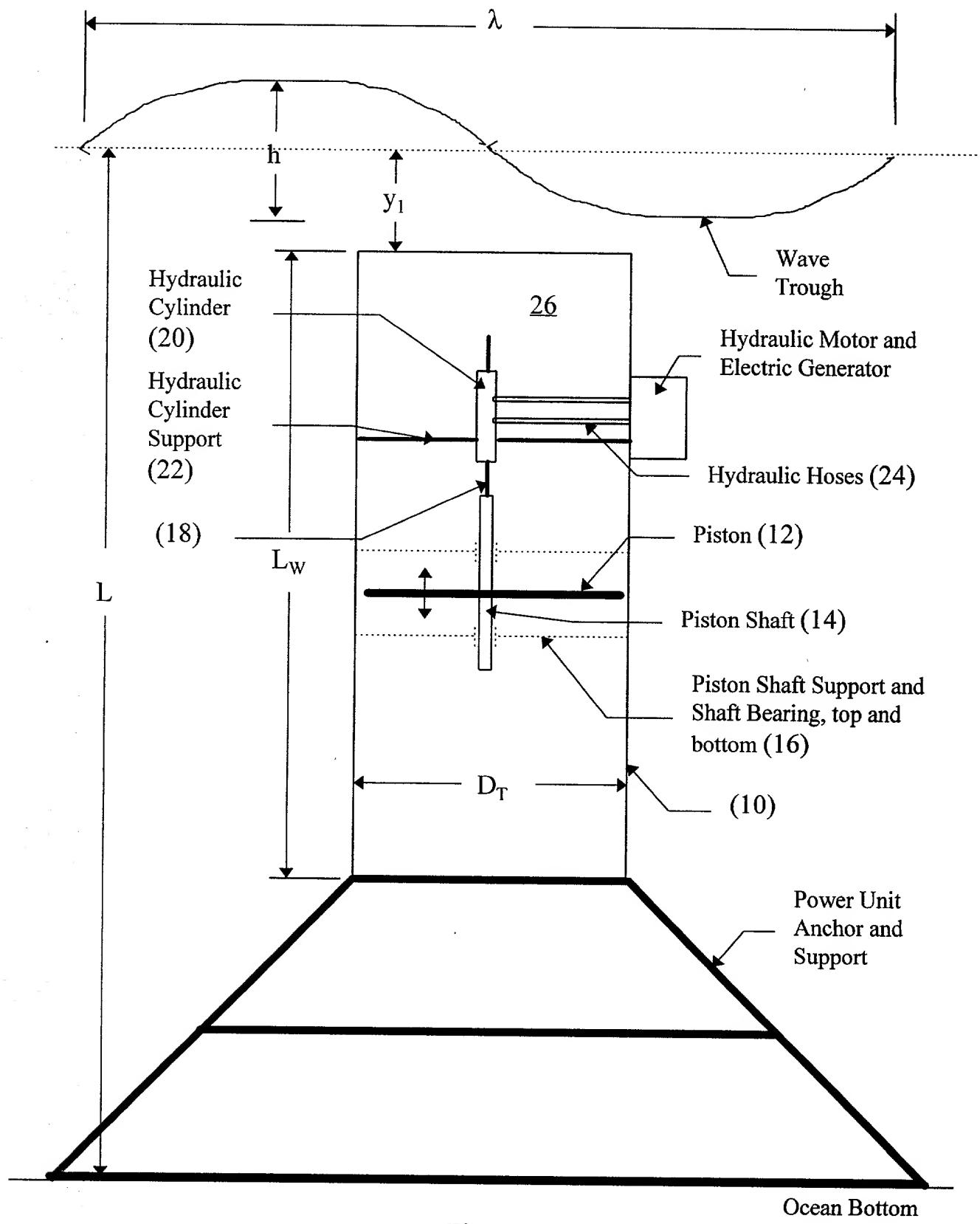


Figure 2

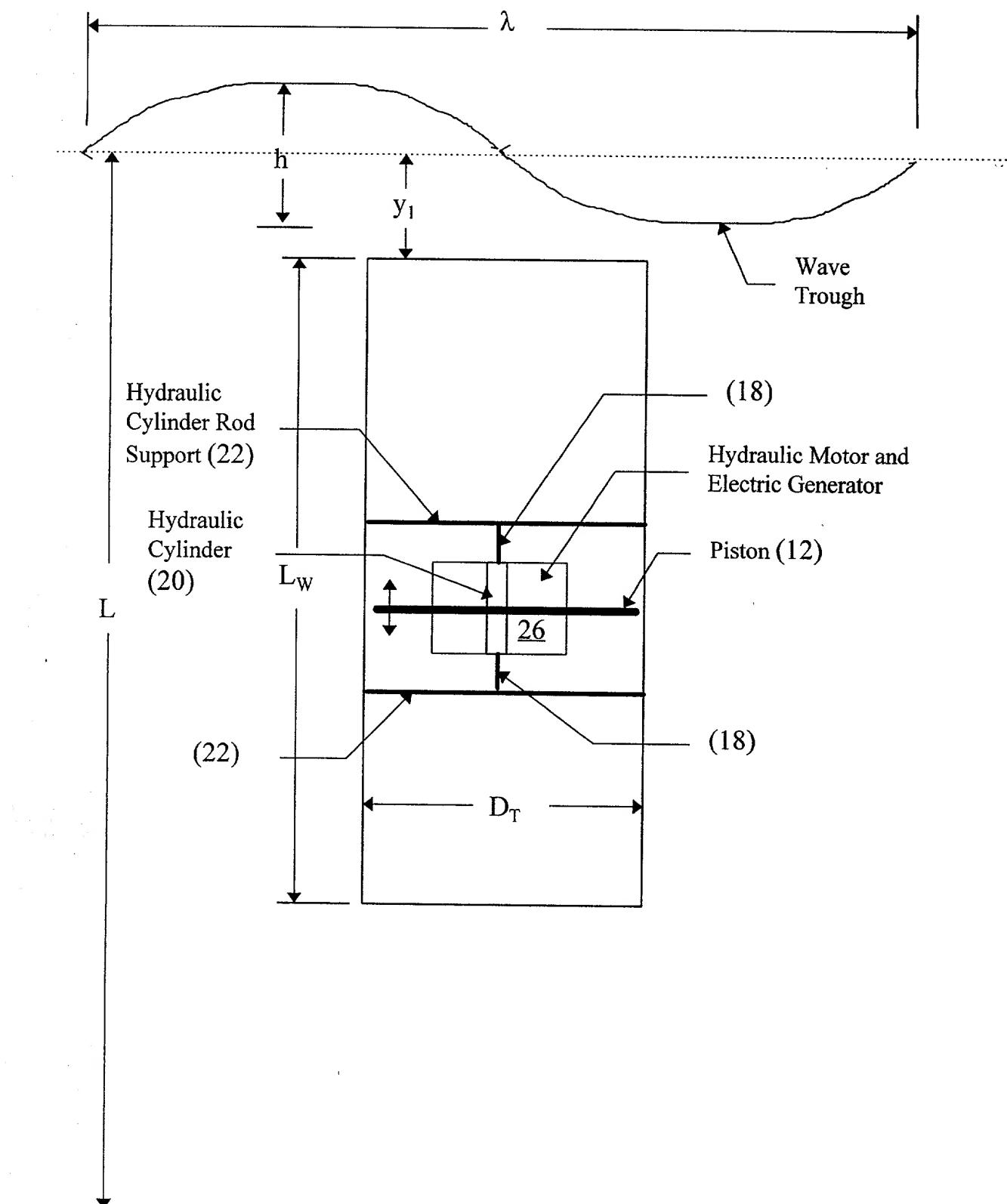


Figure 2A

Ocean Bottom

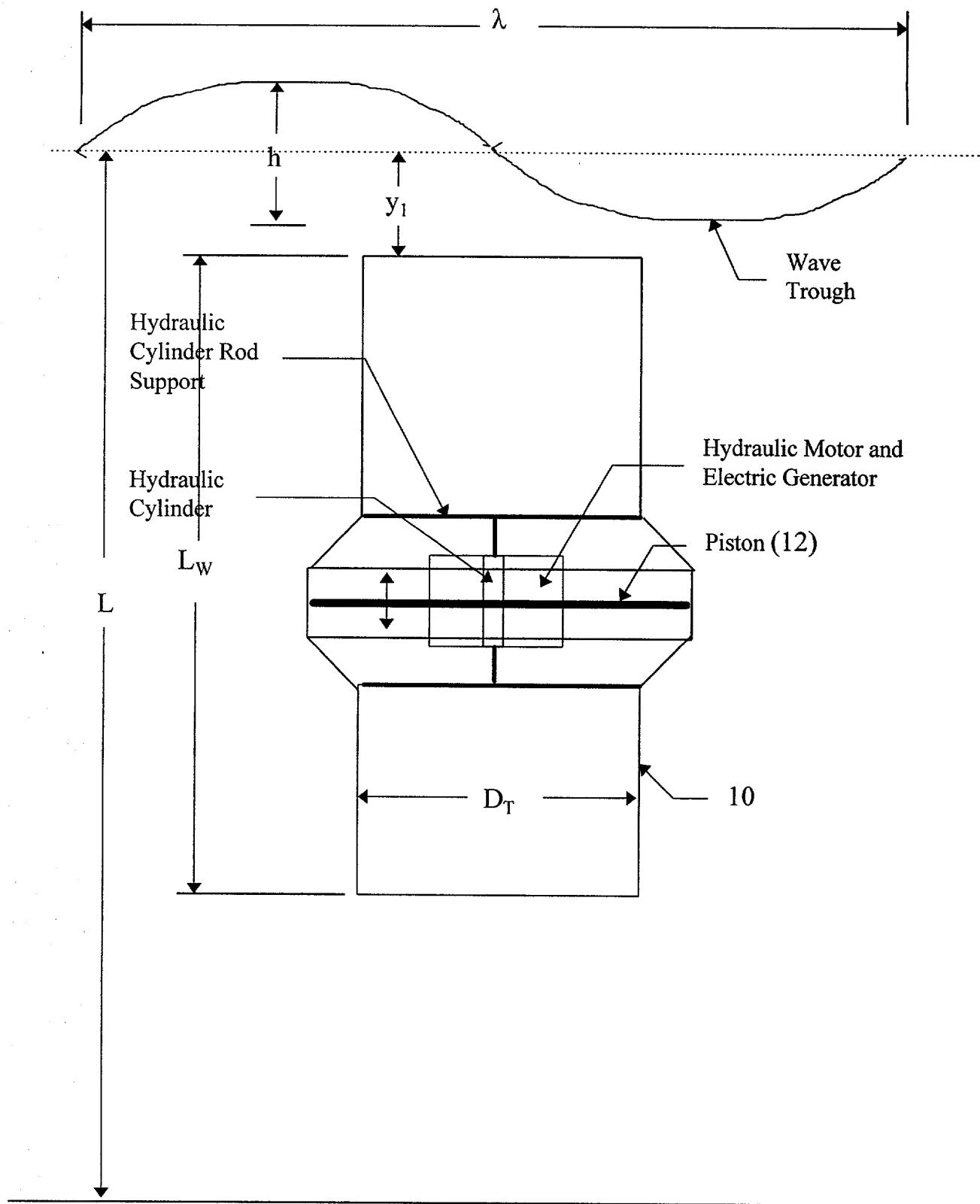


Figure 3

Ocean Bottom

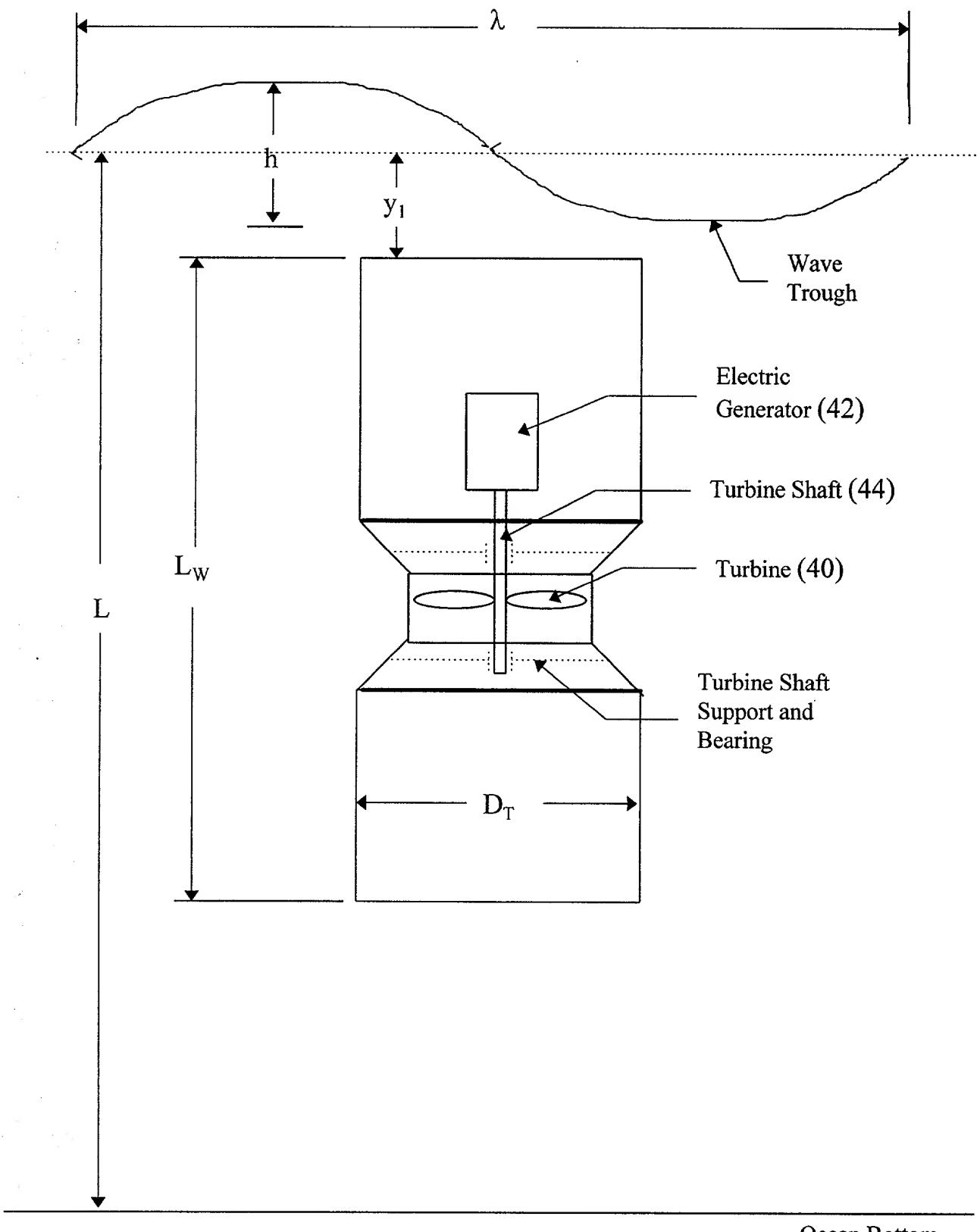


Figure 4

Ocean Bottom

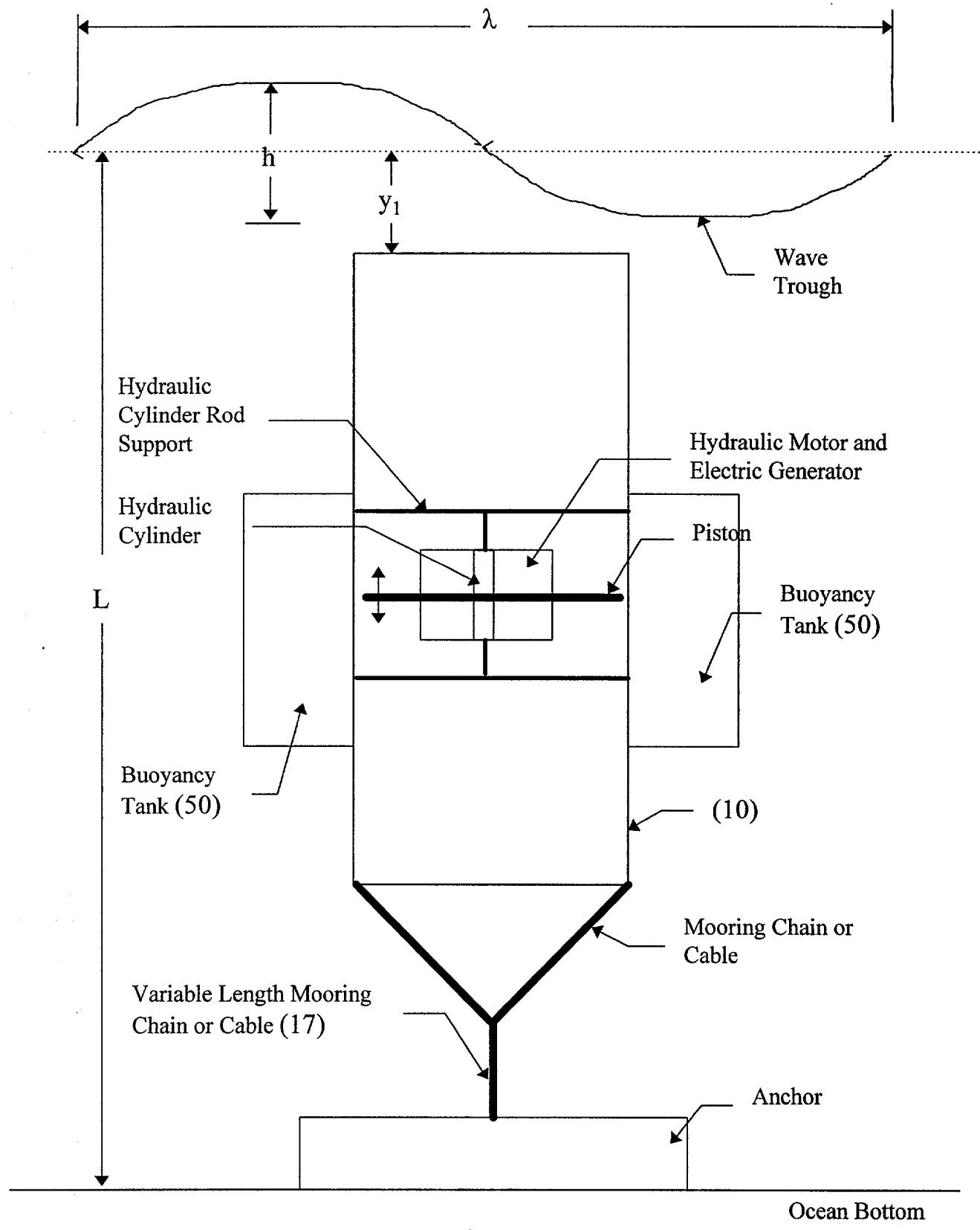


Figure 5

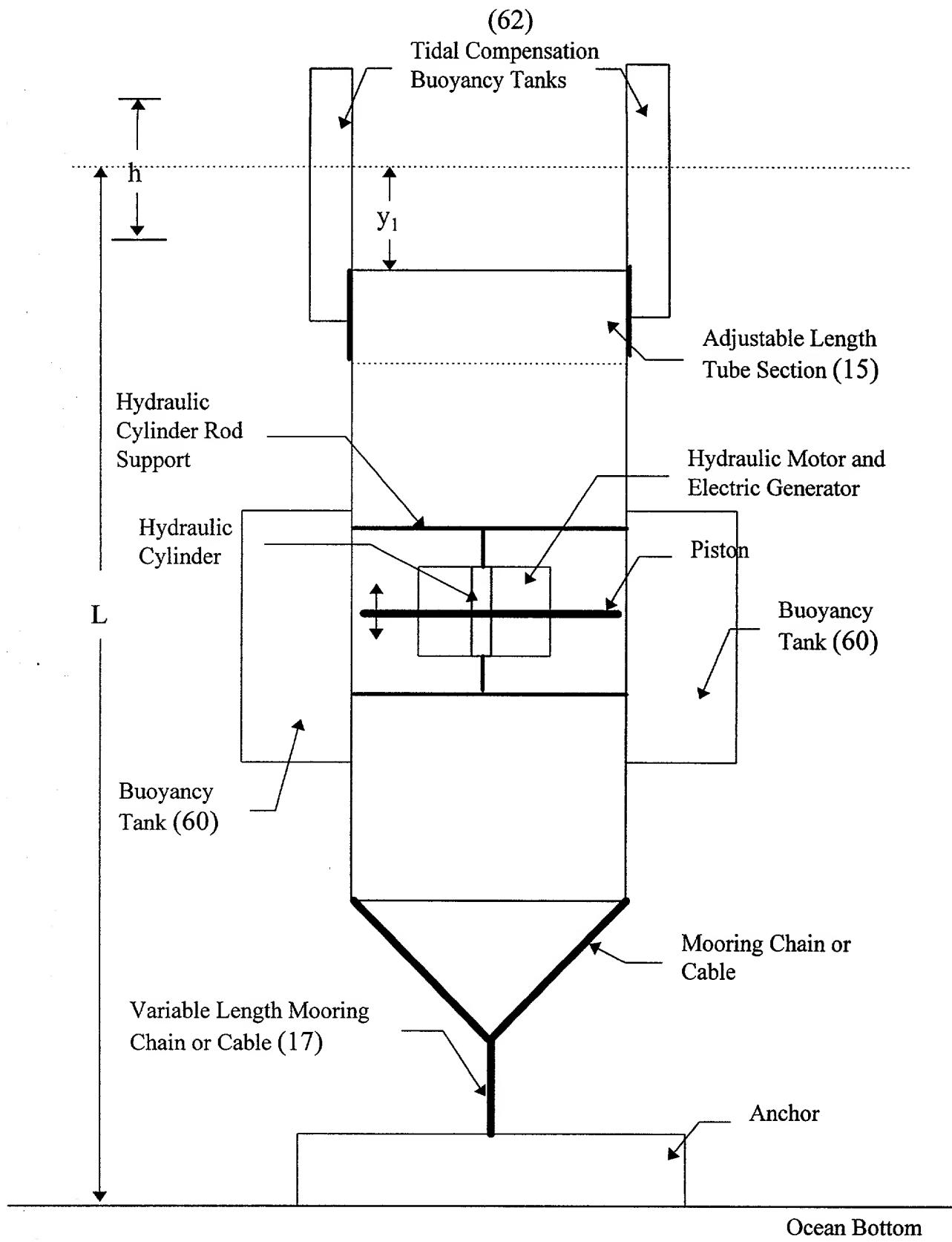


Figure 6

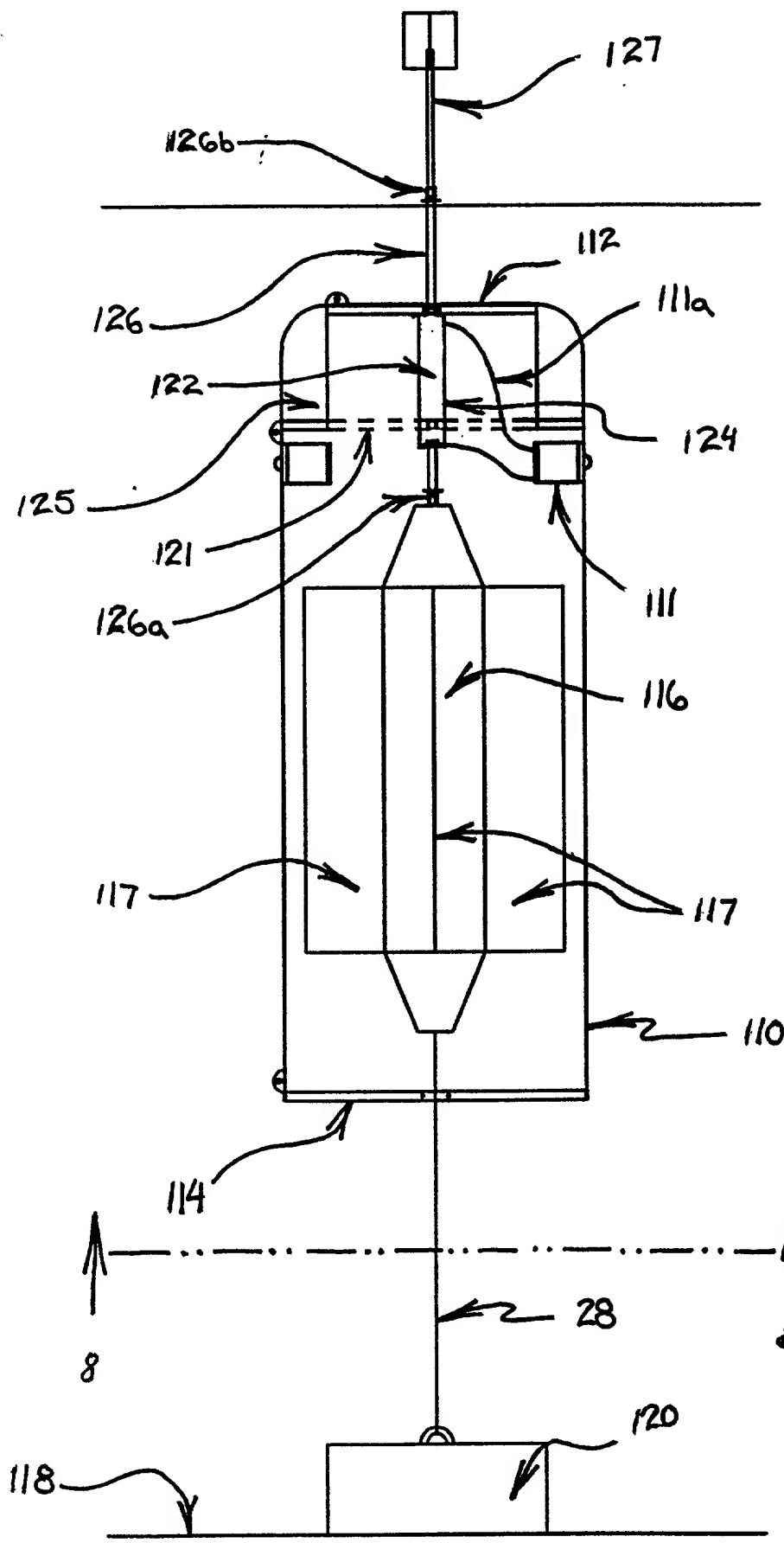


Figure 7.

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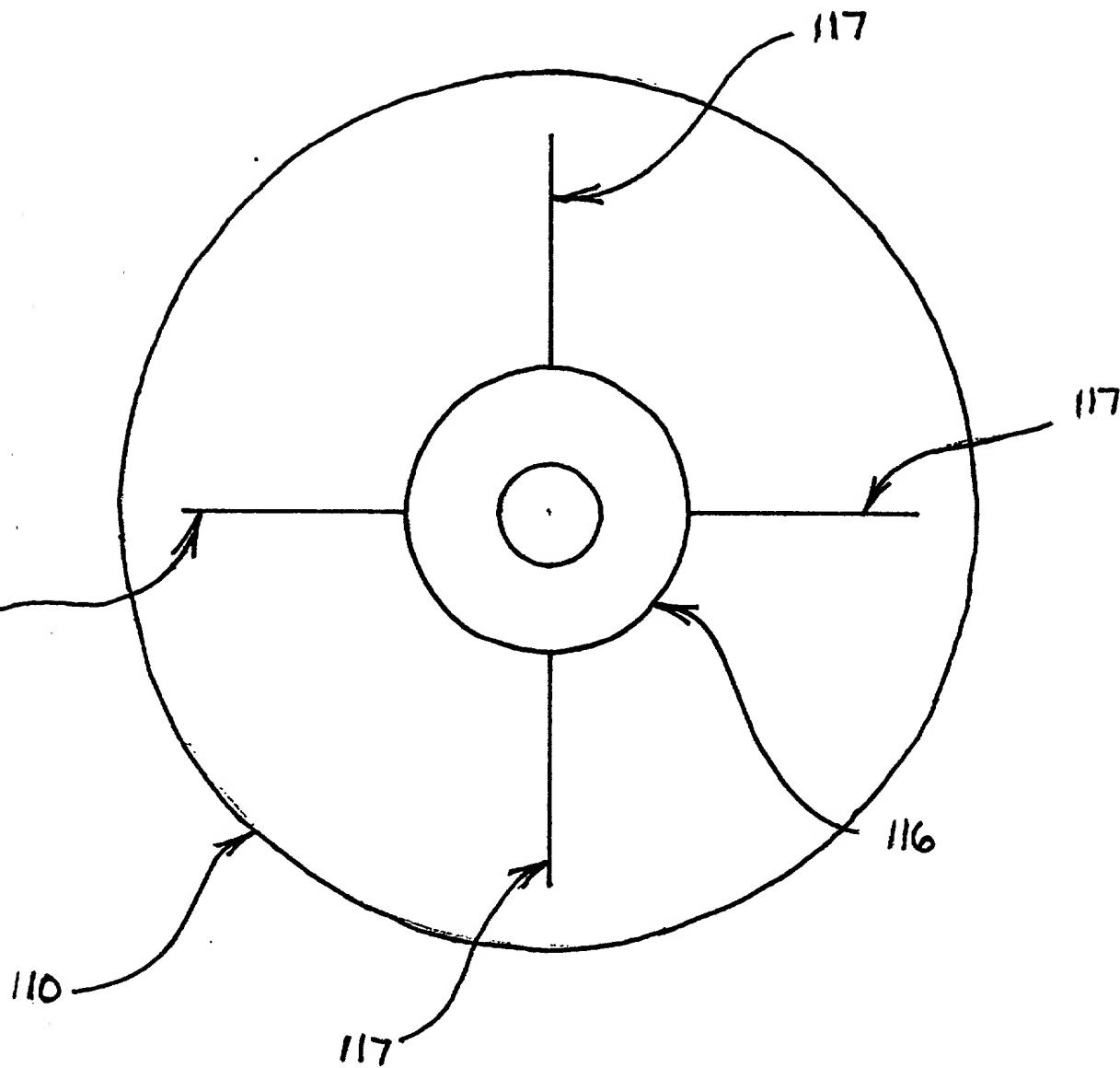


Figure 8

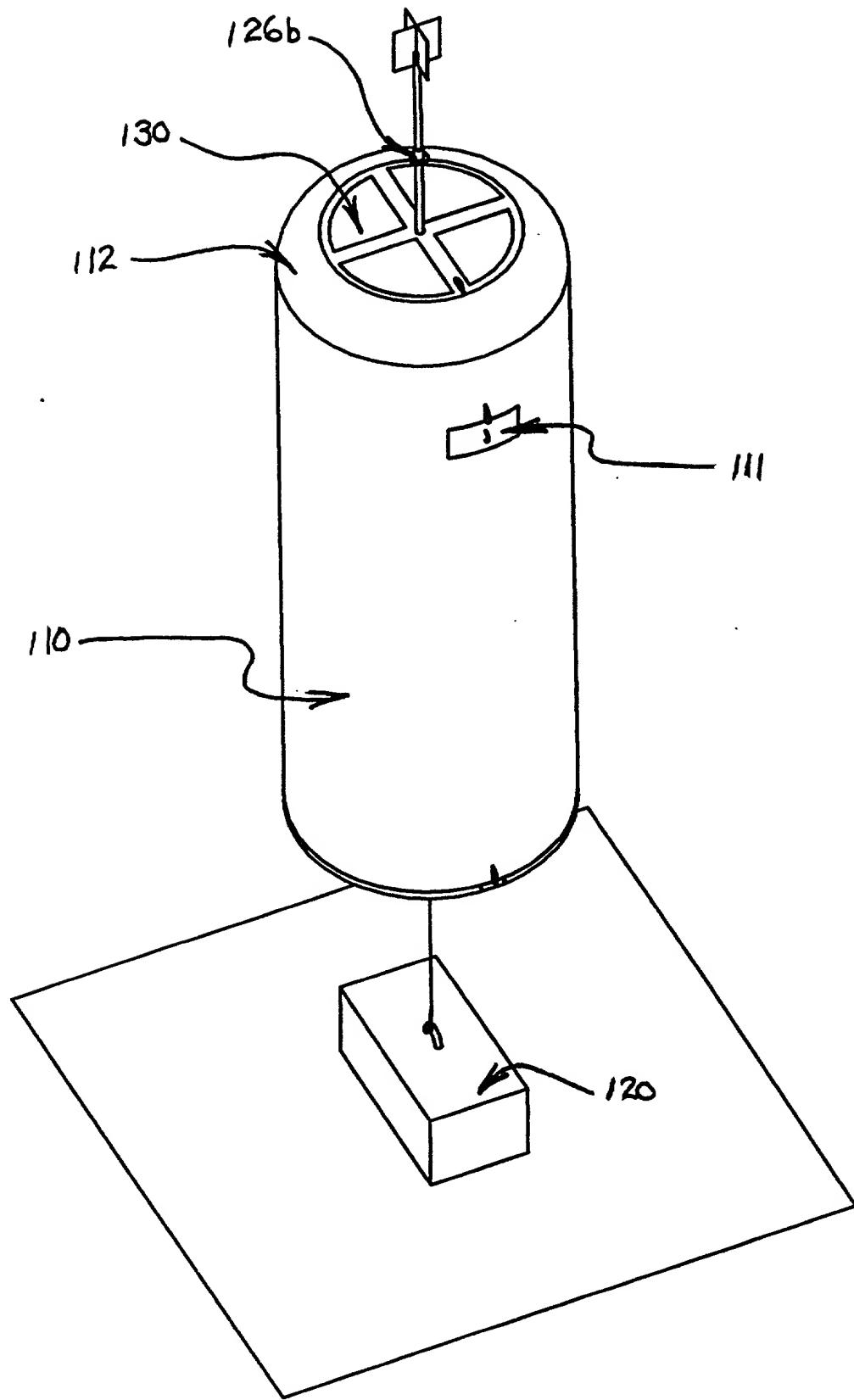


Figure 9

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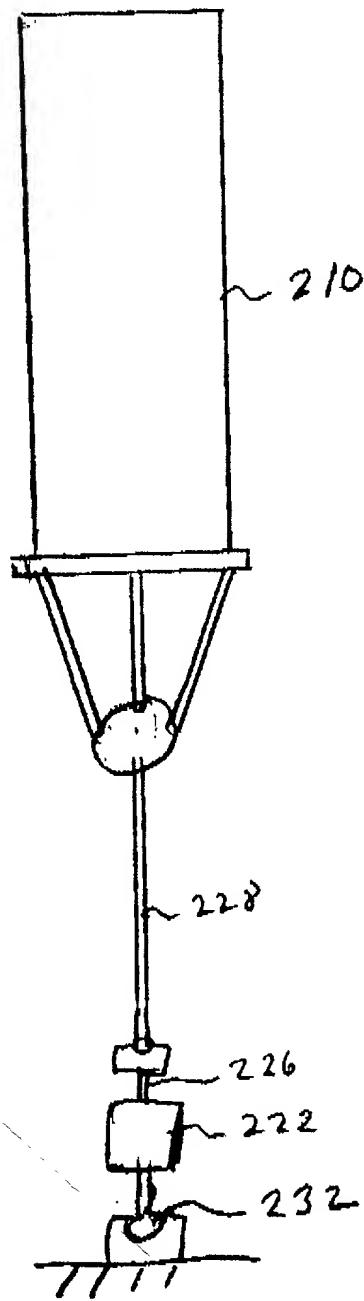


Fig. 10

**IN THE UNITED STATES PATENT AND TRADEMARK OFFICE**

Declaration and Power of Attorney

As a below named inventor, I declare that:

My residence, post office address and citizenship are as stated below next to my name.

I believe I am the original, first and sole inventor of the subject matter which is claimed and for which a patent is sought on the invention entitled, **WAVE ENERGY CONVERTERS UTILIZING PRESSURE DIFFERENCES** the specification of which is enclosed herewith.

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by an amendment, if any, specifically referred to in this oath or declaration.

I acknowledge the duty to disclose all information known to me which is material to patentability as defined in Title 37, Code of Federal Regulations, 1.56.

I hereby claim foreign priority benefits under Title 35, United States Code, 119 of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed:

PCT/US00/14652 filed May 26, 2000

I hereby claim the benefit under Title 35, United States Code, 120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code 112, I acknowledge the duty to disclose all information known to me to be material to patentability as defined in Title 37, Code of Federal Regulations, 1.56 which became available between the filing date of the prior application and the national or PCT international filing date of this application:

60/136,189 FILED ON MAY 27, 1999  
09/379,421 FILED ON AUGUST 21, 1999

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

I hereby appoint the following attorney(s) with full power of substitution and revocation, to prosecute said application, to make alterations and amendments therein, to receive the patent, and to transact all business in the Patent and Trademark Office connected therewith:

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Michael Y. Epstein, Esq.      Reg. No. 21,186

Telephone calls should be made to Henry I. Schanzer at :

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Inventor's  
signature \_\_\_\_\_ Date \_\_\_\_\_

Residence:  
Citizenship:  
Post Office Address:

Full name of second joint inventor: Meredith Bell

Inventor's  
signature Meredith Bell Date 2/28/01 Meredith Bell

Residence: 24 Winthrop Ct. Milford CT 06460 CT  
Citizenship: United States of America  
Post Office Address: 24 Winthrop Ct Milford, CT 06460

Commonwealth of Massachusetts  
County of Suffolk  
Subscribed and sworn to before me  
this 28 day of February 2001

  
Notary Public  
My Commission Expires May 28, 2004

**IN THE UNITED STATES PATENT AND TRADEMARK OFFICE**

**Declaration and Power of Attorney**

As a below named inventor, I declare that:

My residence, post office address and citizenship are as stated below next to my name.

I believe I am the original, first and sole inventor of the subject matter which is claimed and for which a patent is sought on the invention entitled, **WAVE ENERGY CONVERTERS UTILIZING PRESSURE DIFFERENCES** the specification of which is enclosed herewith.

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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

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**Full name of second joint inventor:** Meredith Bell

Inventor's  
signature \_\_\_\_\_ Date \_\_\_\_\_

Residence:

Citizenship:

Post Office Address: